

Combining SOFC Technology for Electrolysis  
with CO<sub>2</sub> Recycling as an Approach to Hydrogen Storage  
Session GHT44a H<sub>2</sub> Production  
Thursday, 19 November 2009  
4:00-6:00 PM



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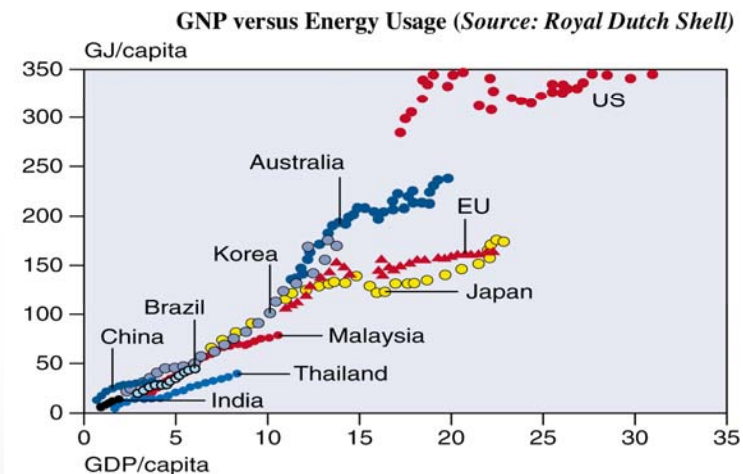
J. Hartvigsen, S. Elangovan, A. Nickens, L. Frost – Ceramatec, Inc.  
C. Stoots, J. O'Brien, J.S. Herring – Idaho National Laboratory



**November 16-19, 2009 Palm Springs Convention Center, Palm Springs, CA, USA**

# Energy, Environment & Economy

- Environment
  - Climate Change
    - GHG sources
      - 8 tons CO<sub>2</sub>/kW-yr from coal or oil
      - Leaky natural gas pipelines
      - Ruminants
    - Ozone hole - no, that's a different topic
  - Habitat Impacts
    - Drilling in Arctic National Wildlife Refuge
    - Wind turbines in Chesapeake Bay
  - Air pollution
- Limited Resources
  - Oil
    - National security
  - Gas
    - Heating vs. power generation
    - Transportation issues
  - Renewables
- Energy as the key to prosperity



# Why Electrolytic Synfuels

- Electrolysis efficiency
- Energy storage density
- Fits in existing distribution infrastructure
- Synergy with intermittent energy sources
- No added CO<sub>2</sub> emissions
- Reduced work of compression
- Compatible with existing vehicle fleet
  - 20 to 50 year crossover



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# Storing Hydrogen With CO<sub>2</sub>

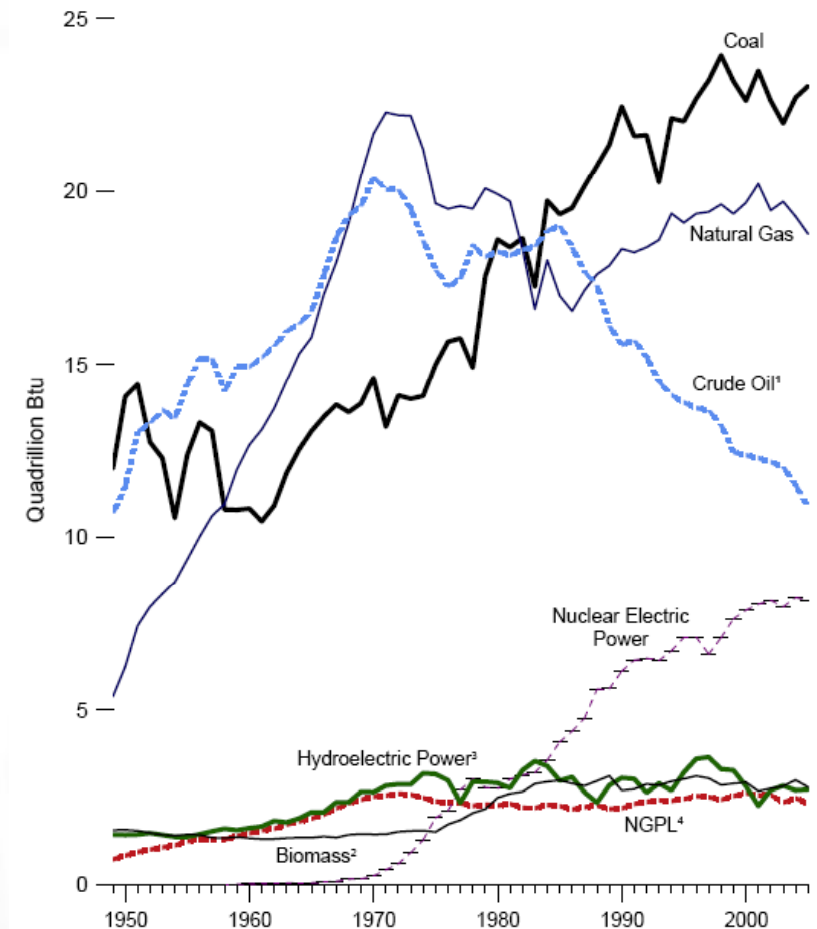
- Energy Sources
  - Wind, Solar (PV & heat), Hydro, Nuclear
- Carbon Sources
  - Metallurgical Reduction, Cement Kilns
  - Fermentation, Digester gas
  - Biomass gasifiers
  - Fossil Power Systems
- Conversion Technology
  - SOFC electrolyzer, steam+CO<sub>2</sub>=> syngas
- Products
  - SNG, Fischer Tropsch liquids



# Carbon Free Energy Source Options

- Hydrogen production from electrolysis
  - High temperature 29 tons/GW-hr
  - Conventional 21 tons/GW-hr
- Renewable energy resources
  - Large Scale Wind
    - 800 GW at class 4+ US wind sites
  - Small Hydro
    - 70GW new at existing dams (Chu 22 Sep09)
  - Concentrator Photovoltaic
    - Land area 12km<sup>2</sup> /GW
  - Biomass
    - Ag/Forestry byproduct
    - Carbon neutral cycle assuming production and processing are carbon free
- Nuclear
  - 25 new plants announced
  - Increased output of existing units
    - Note trend in figure since 1970

By Major Source, 1949-2005



<sup>1</sup> Includes lease condensate.  
<sup>2</sup> Wood, waste, and alcohol fuels (ethanol blended into motor gasoline).  
<sup>3</sup> Conventional hydroelectric power.  
<sup>4</sup> Natural gas plant liquids.

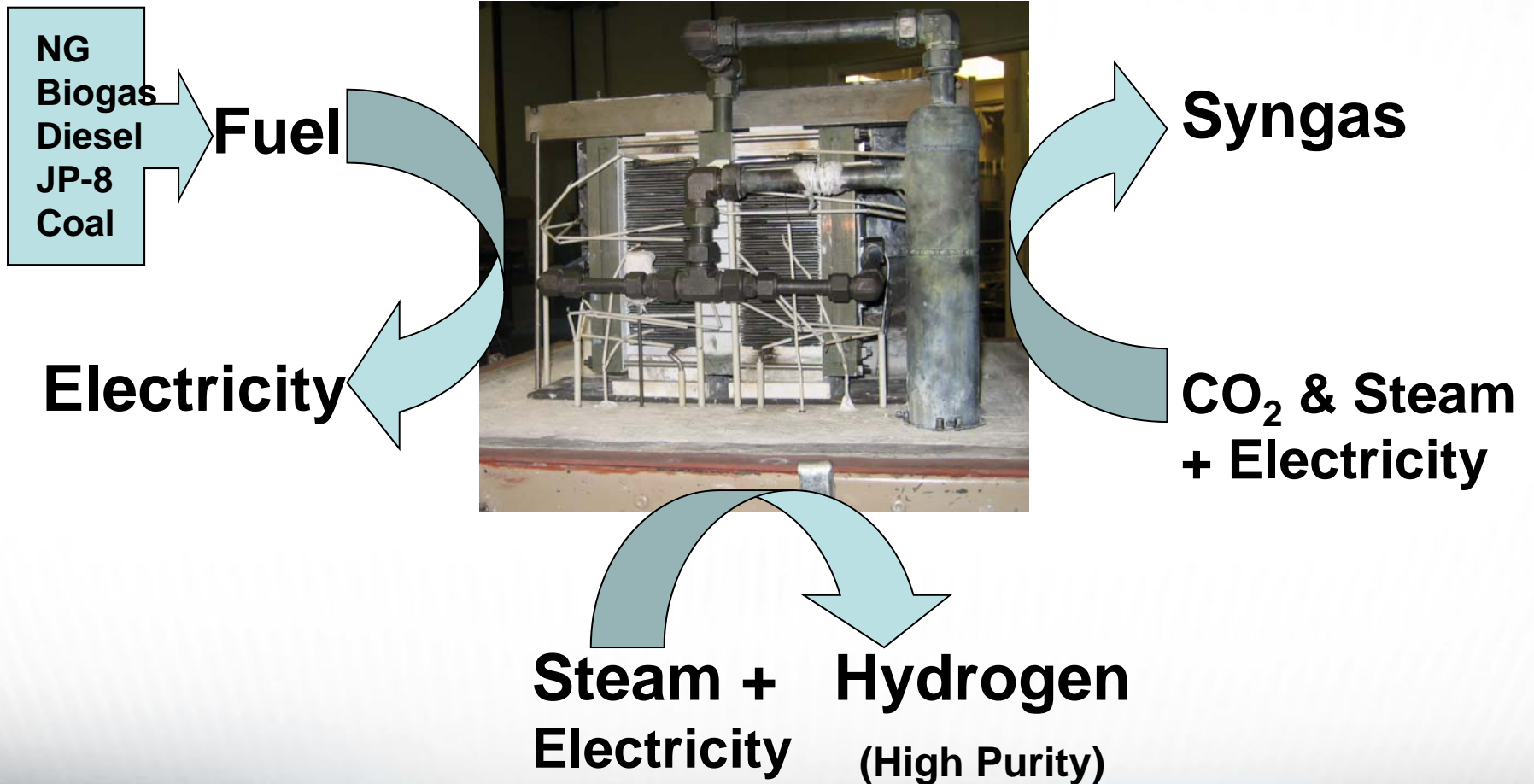
[http://www.eia.doe.gov/emeu/aer/pdf/pages/sec1\\_6.pdf](http://www.eia.doe.gov/emeu/aer/pdf/pages/sec1_6.pdf)



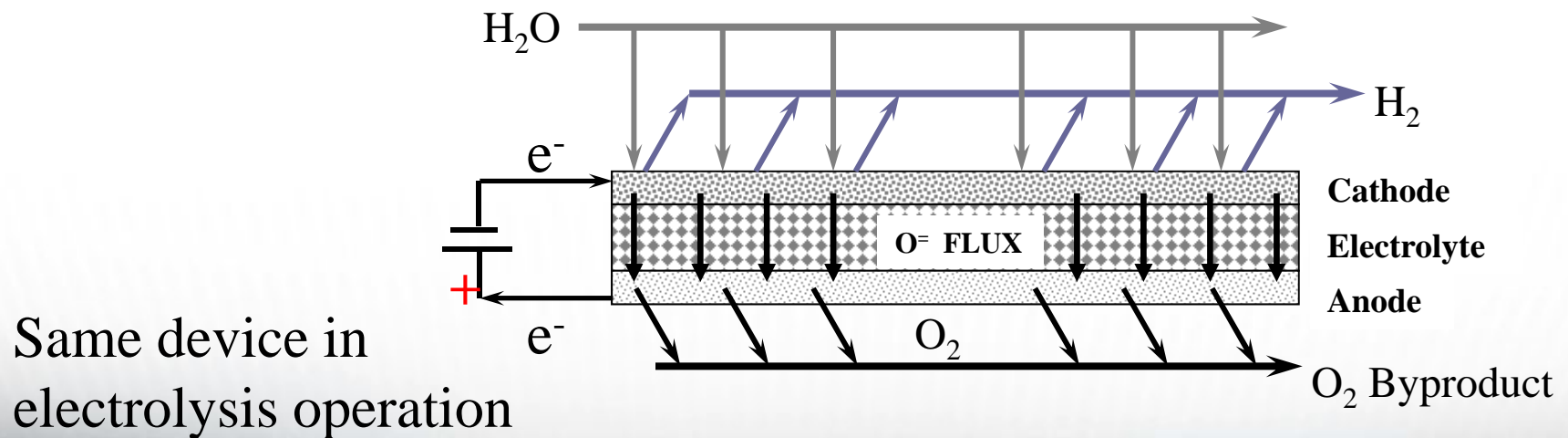
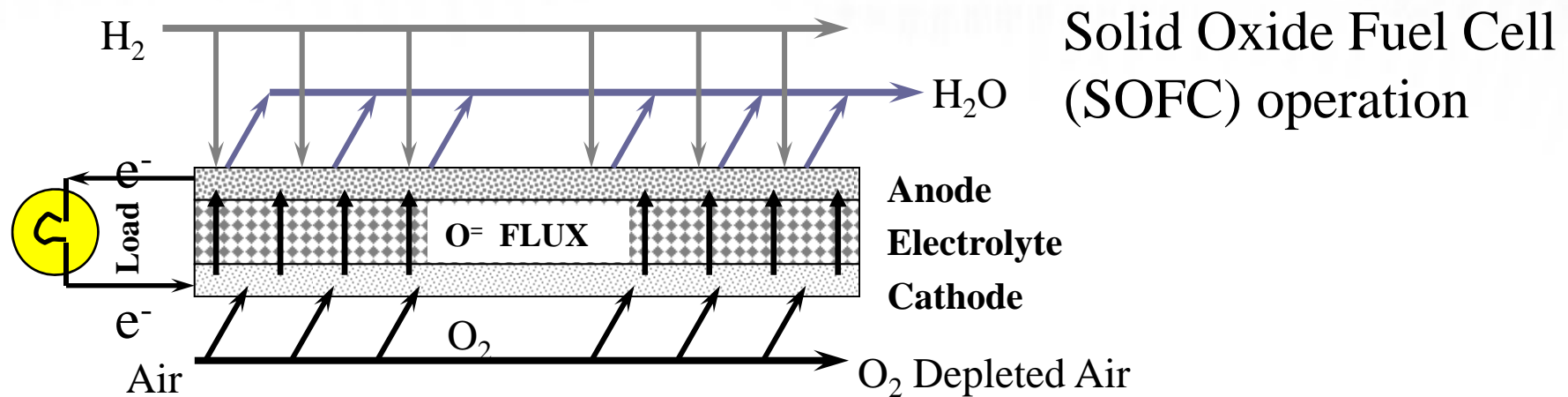
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# One Technology - Multiple Modes Of Operation

## Solid Oxide Stack Module



# Steam Electrolysis Operating Principle

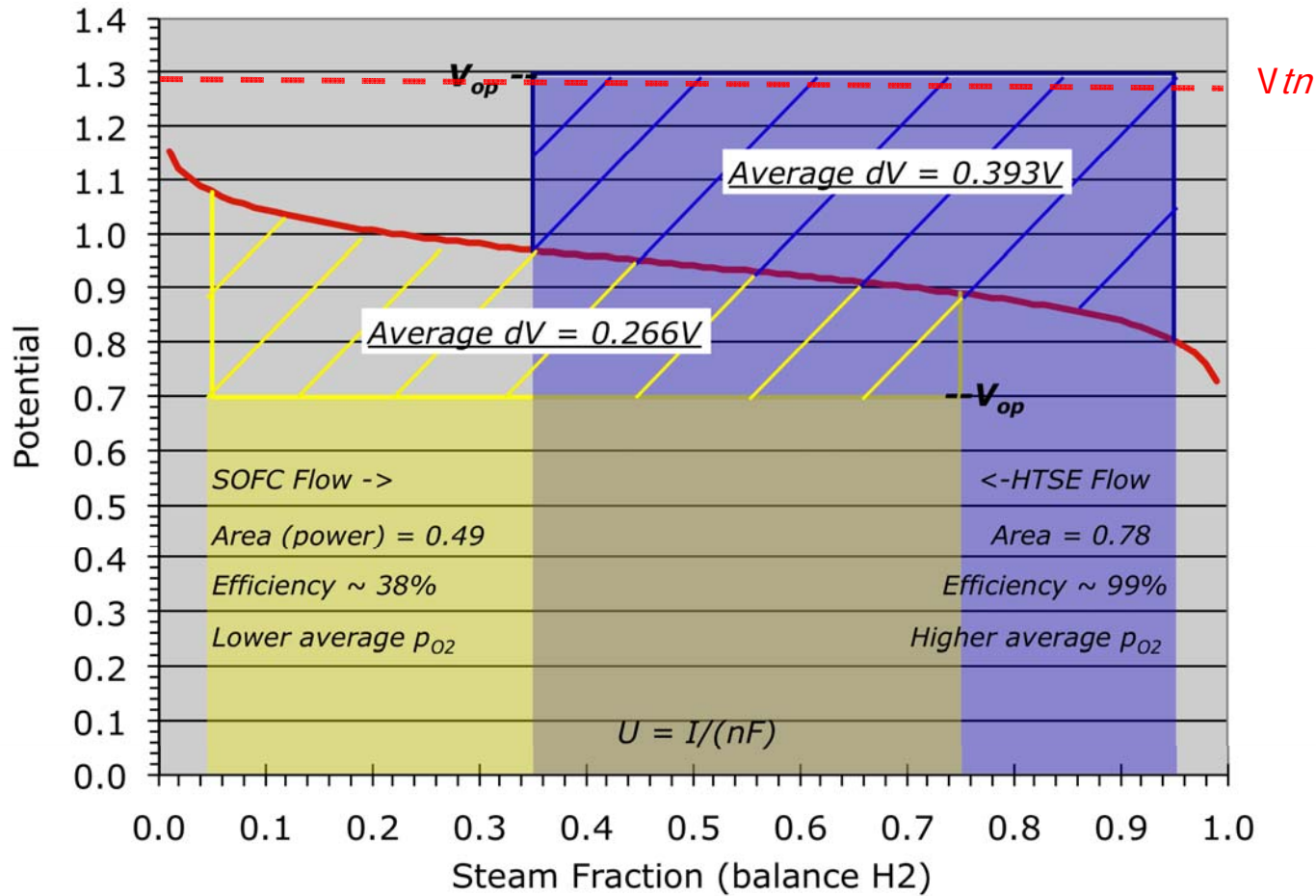


# SOFC vs. SOEC Cell & Stack Designs

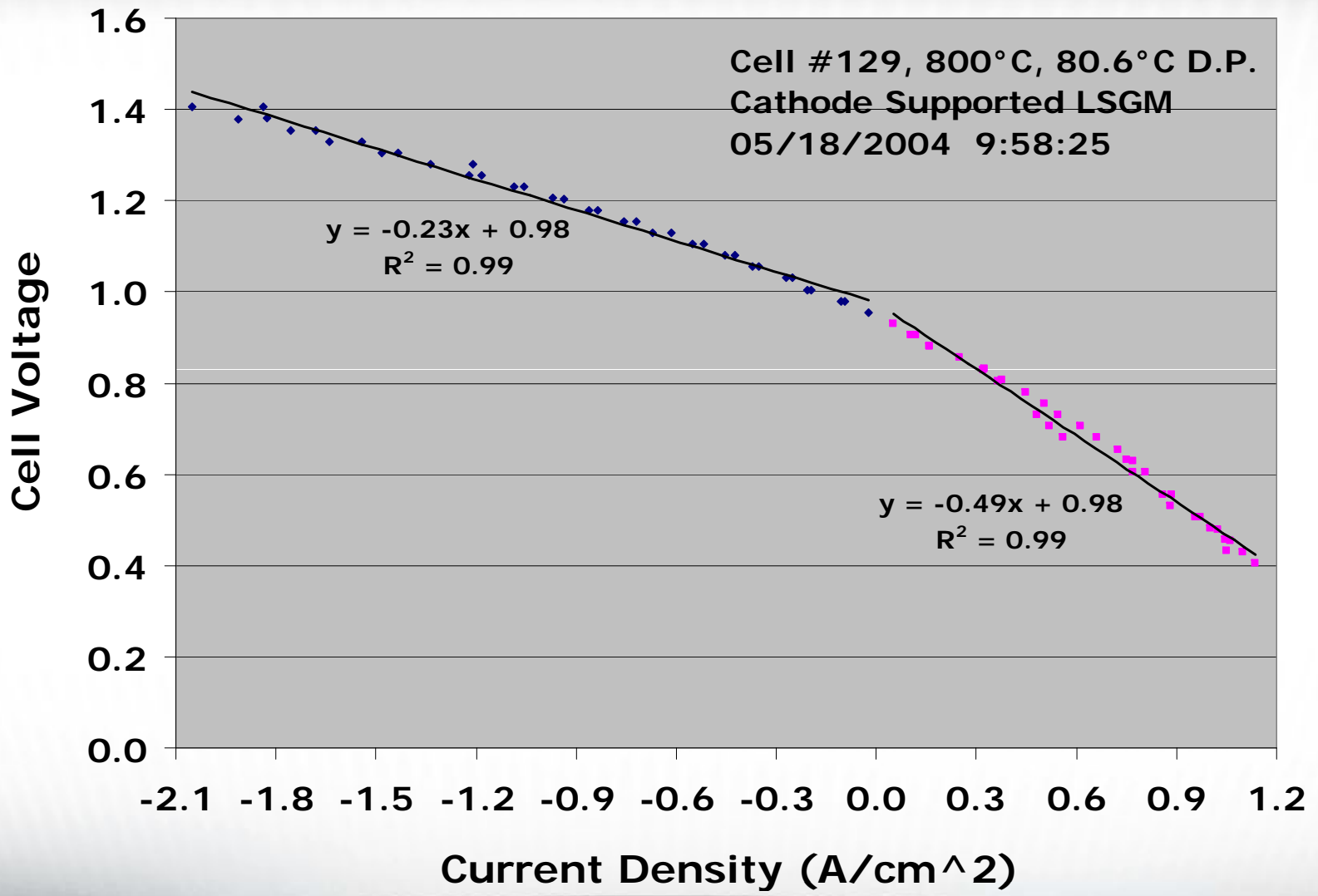
- Cells are virtually identical
  - Same electrolyte, electrodes, pattern, etc.
  - Oxygen evolution creates asymmetry in oxygen electrode supported SOEC
  - Opposite effect exhibited in hydrogen electrode supported SOFC
- SOEC seals more challenging
  - Higher back pressure on seals due to product collection vs. burner
  - Low molecular weight stream vs. reformat
    - Diffusion mechanism more active relative to hydrodynamic
    - Hydrogen permeation in metal icon destabilizes air side scale
- SOEC is more corrosive environment
  - High steam content
  - High oxygen concentration
  - Coating changes and seal compatibility study (glass fluxes scale)
- Potential icon design differences due to
  - Design air channels for heat rejection or injection (channel size)
  - SOEC has potential for very large cell areas



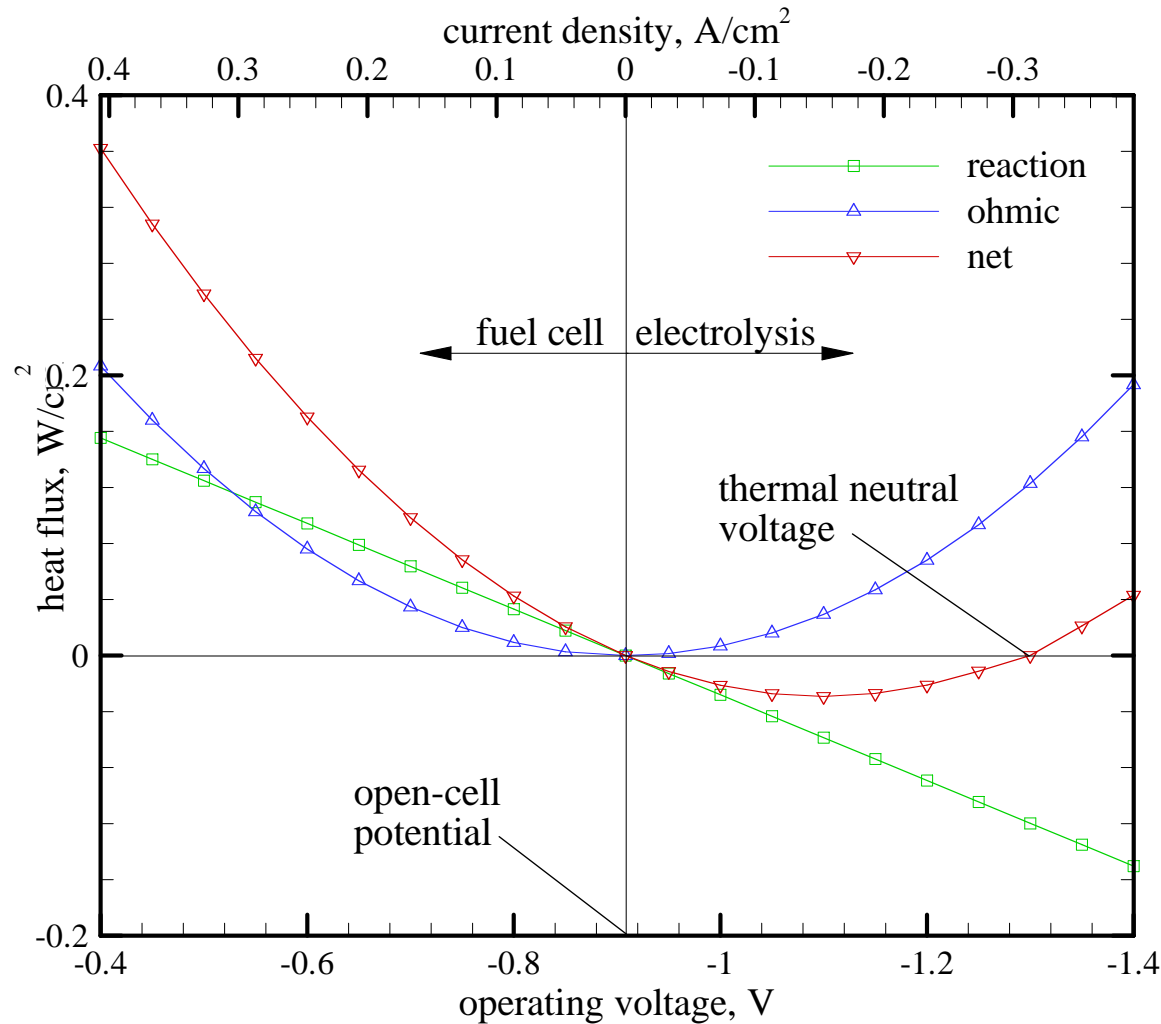
# SOFC-SOEC Contrasts in (V:X<sub>i</sub>) Space



# Polarization of Oxygen Electrode Supported Cell



# Energy of fuel-cell vs. electrolysis mode



Stack ASR = 1.25,  
 T = 927 C,  
 $y_{H_2,i} = 0.1$ ,  
 $y_{H_2,o} = 0.95$

$$V_{tn} = \frac{-\Delta h_R}{2F}$$

(1.291 V at 1200 K)



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# Typical SOEC and SOFC Temperature Maps

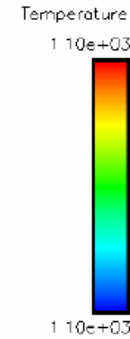
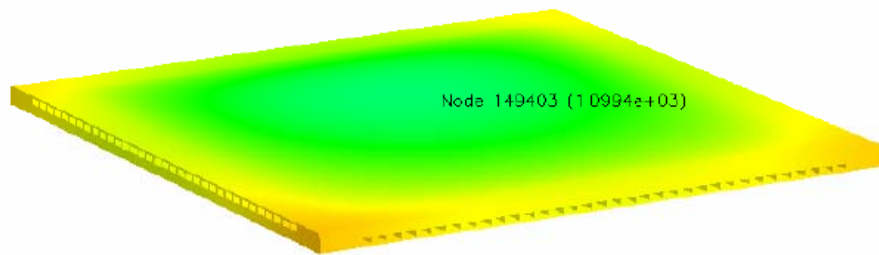
min: 1.10e+03, node 147497  
max: 1.10e+03, node 114234

$V_{op} = 1.288 \text{ V}$

$I = 21.37 \text{ A}$

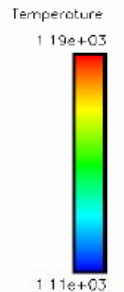
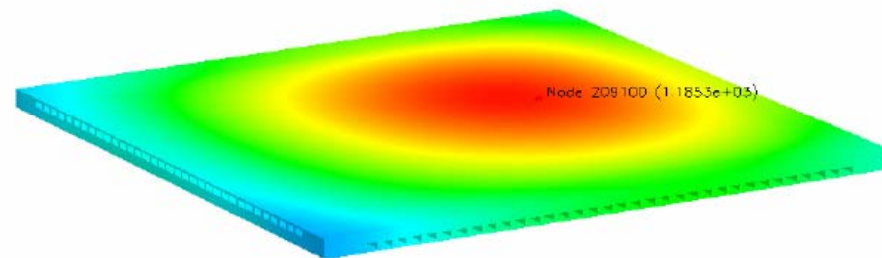
$T = 1100 \text{ K}$

Feed:  $\text{H}_2\text{O}:\text{H}_2$  90:10  $4.39\text{e-}6 \text{ mol/sec-channel}$   
10% of SOFC Air  $4.2\text{e-}6 \text{ mol/sec-channel}$



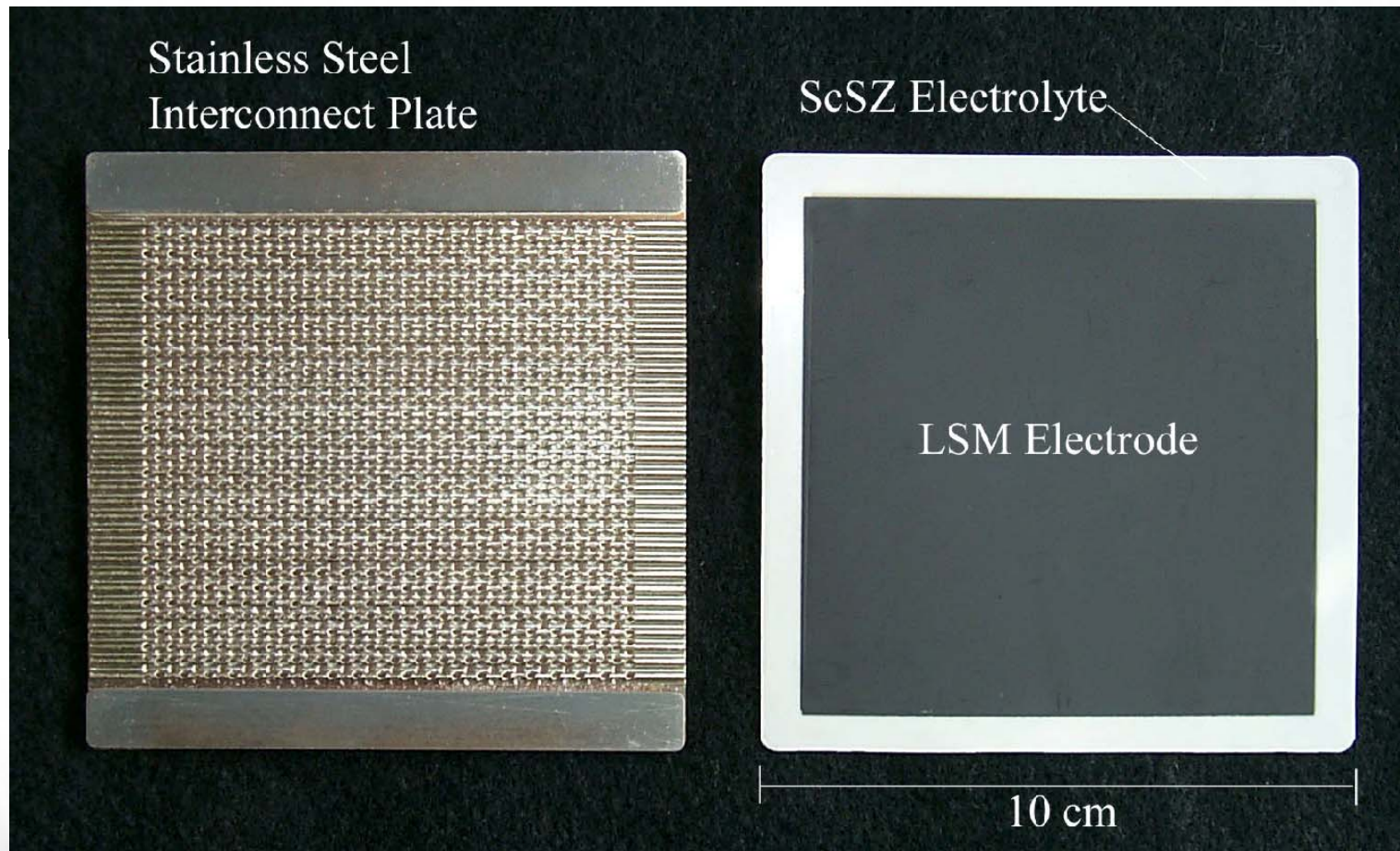
Isothermal

SOFC  $\Delta T > 90^\circ\text{C}$   
Resistance doubling  $\sim 67^\circ\text{C}$   
Thermal expansion issues



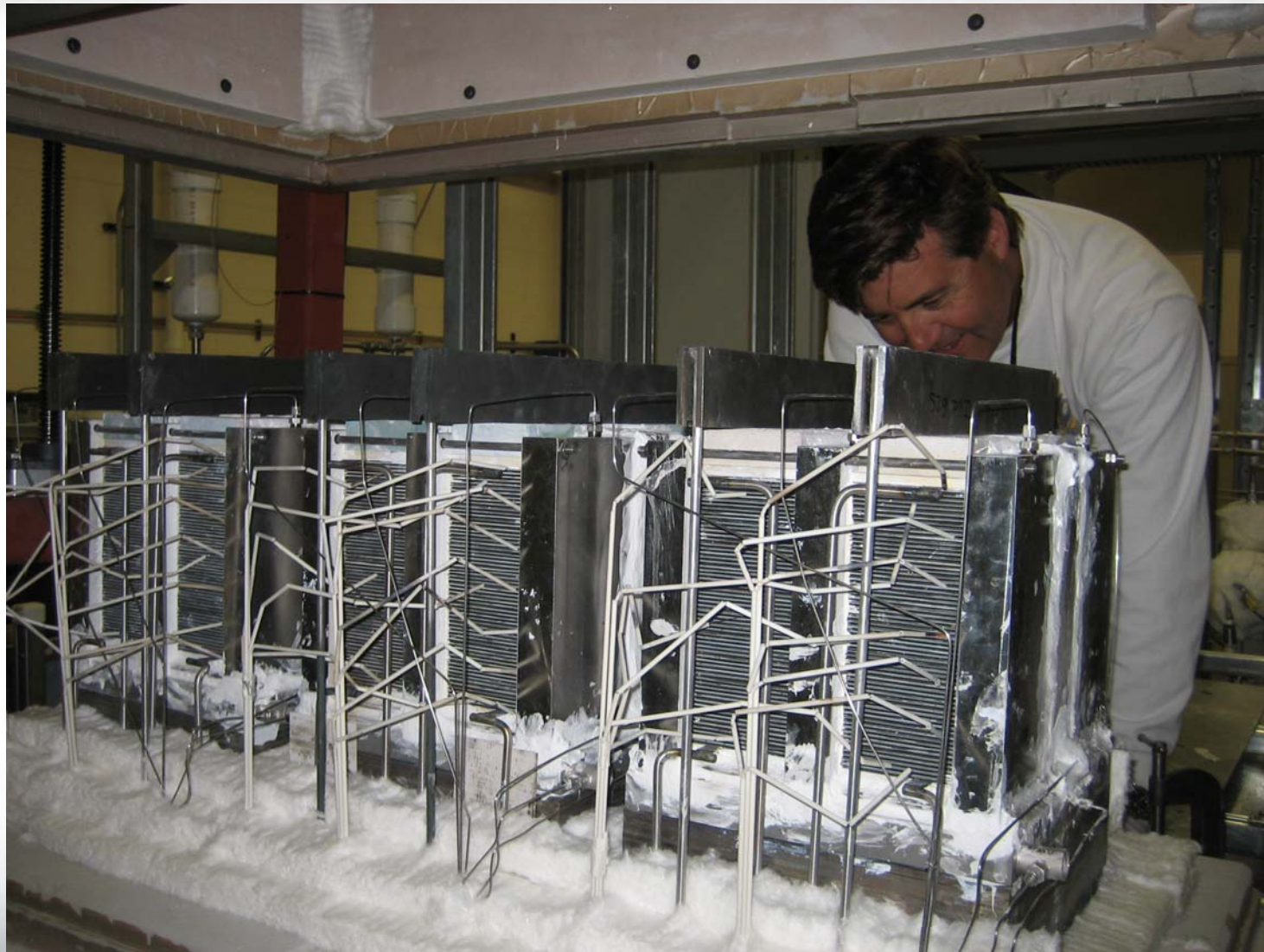
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# Stack Components



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# ILS System 5.7Nm<sup>3</sup>/hr, 18kW H<sub>2</sub> Rate



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# Electrolysis Cells at 20cm Scale



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# Electrolysis Module in Operation



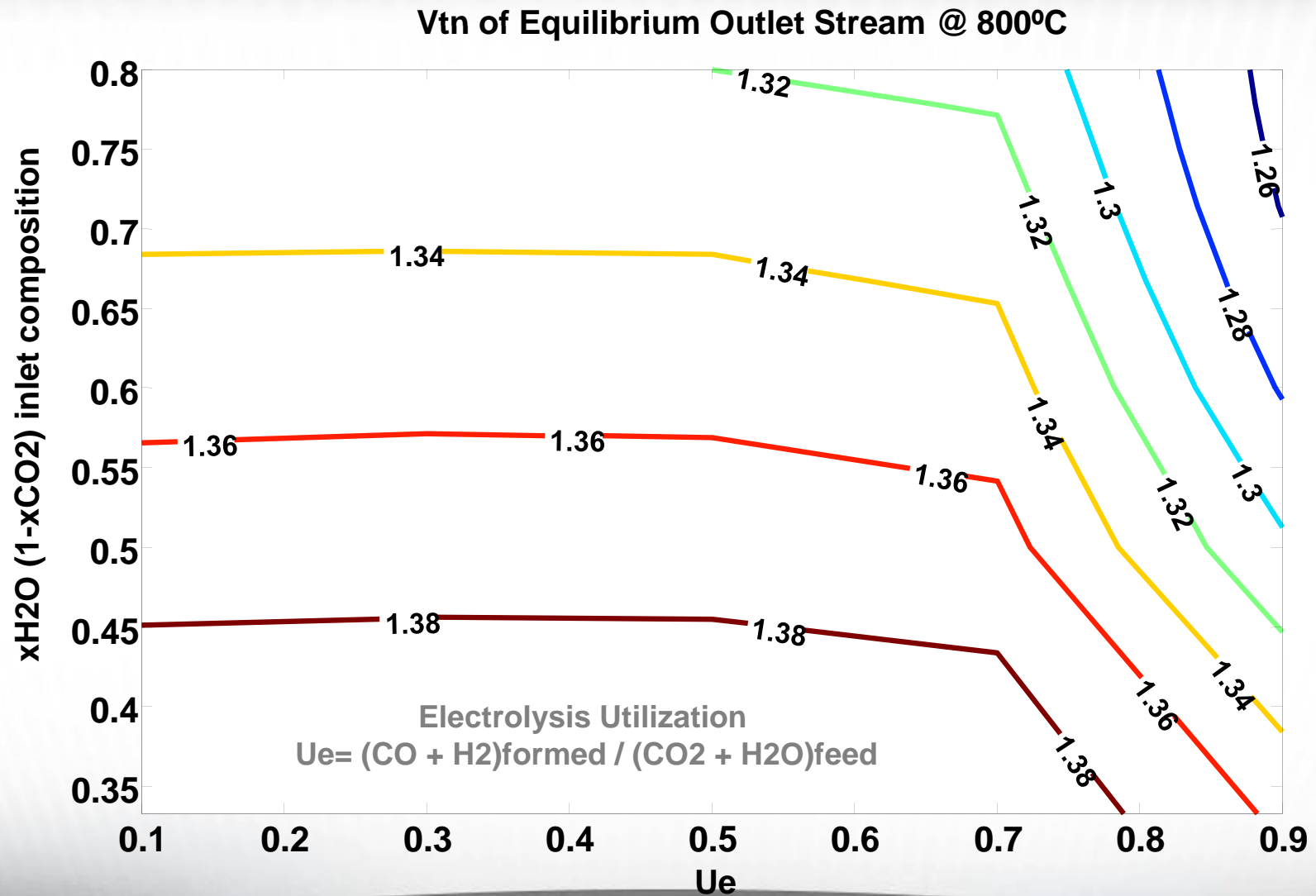
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# INL Internally Funded CO<sub>2</sub> Electrolysis Project

- Button cell testing
  - Gas analysis
    - INL – using CO<sub>2</sub> sensors
    - Ceramatec – micro-channel GC
- Analysis
  - Thermodynamic parameters
    - Thermal Neutral Voltage
    - CO & CO<sub>2</sub> reduction potentials
  - System process model
- Electro-kinetics of steam/hydrogen vs. CO/CO<sub>2</sub> reactions
  - Dry CO/CO<sub>2</sub>
  - Wet (CO<sub>2</sub>/H<sub>2</sub>)
  - Wet to dry transient



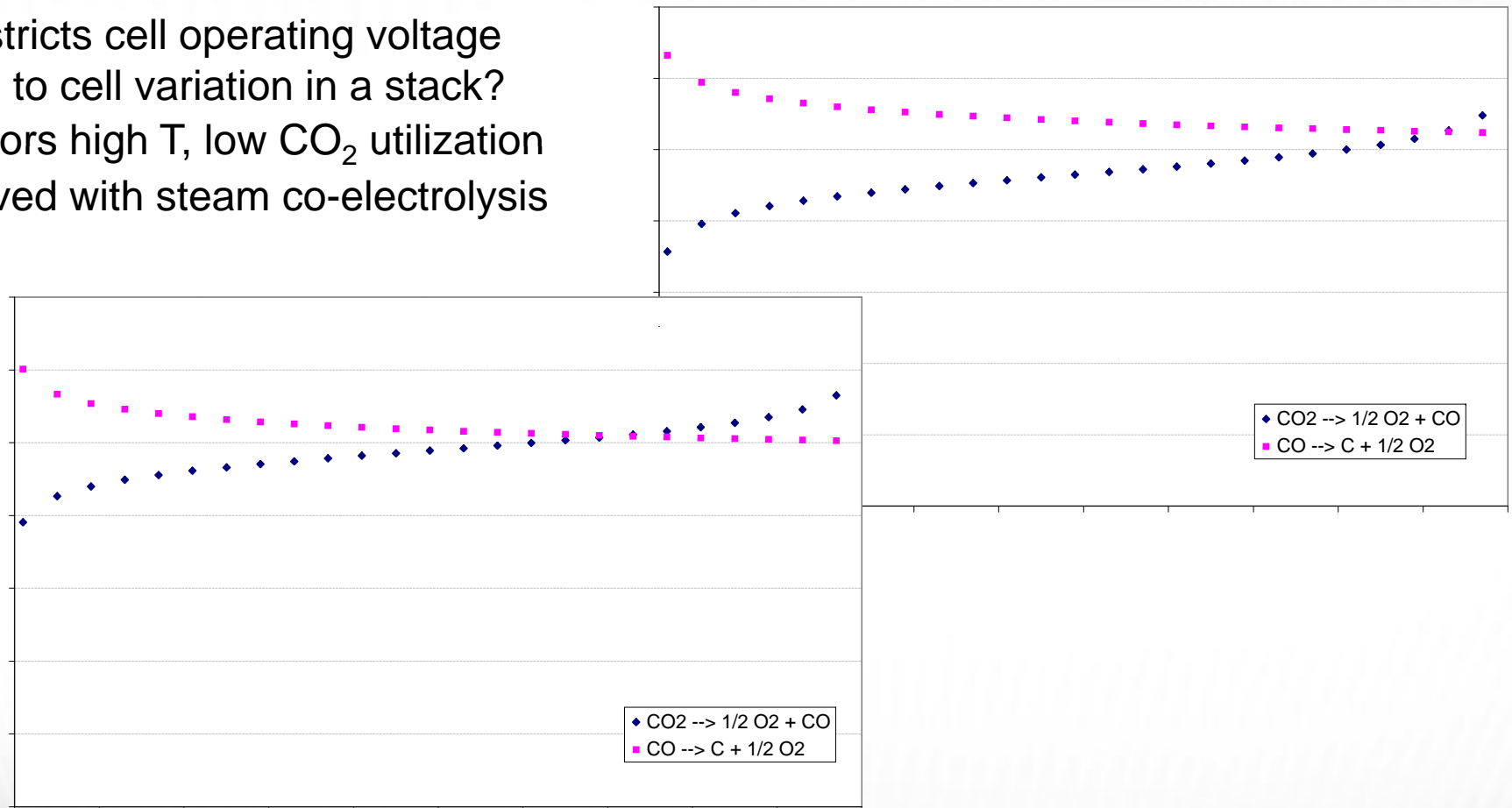
# Co-Electrolysis Thermal Neutral Voltage Map



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# Reduction Potentials of CO<sub>2</sub> and CO

Restricts cell operating voltage  
Cell to cell variation in a stack?  
Favors high T, low CO<sub>2</sub> utilization  
Solved with steam co-electrolysis



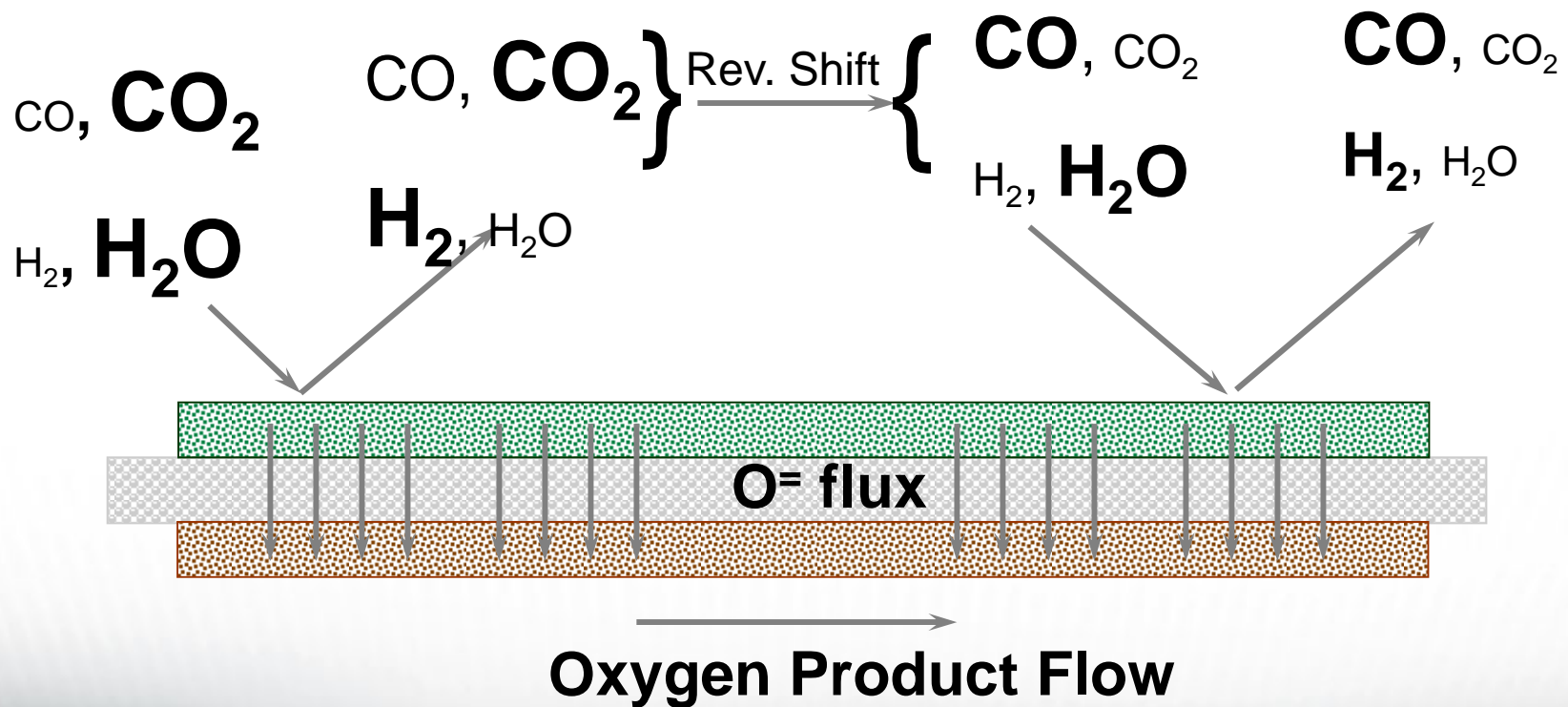
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# Reverse Shift & Electrolysis Of CO<sub>2</sub>

**Feed: H<sub>2</sub>O, CO<sub>2</sub>, (minor H<sub>2</sub>, CO)**

**Reverse Shift Reaction: CO<sub>2</sub> + ↑↑ H<sub>2</sub> <==> CO + ↓↓ H<sub>2</sub>O**

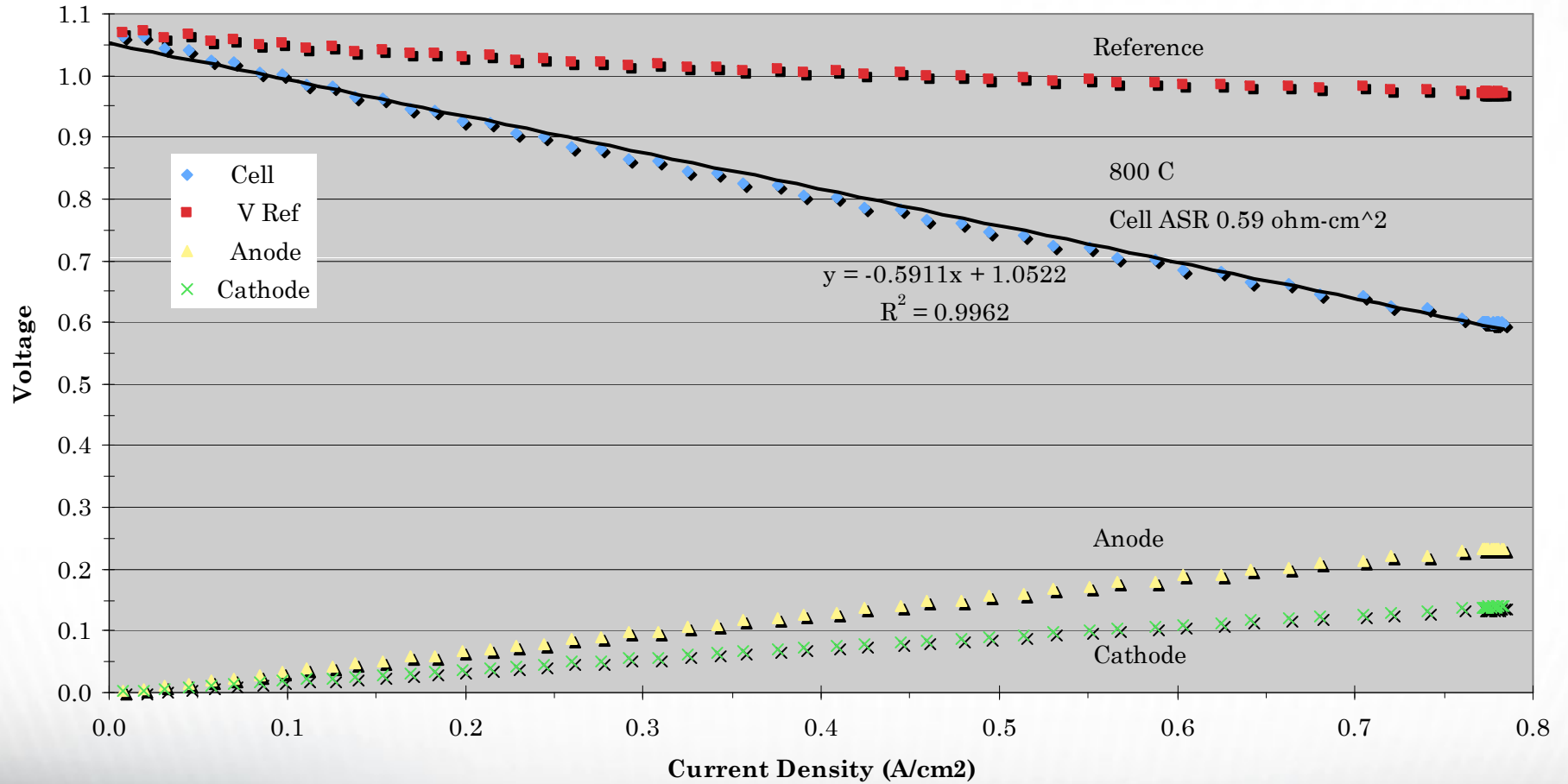
**As steam is consumed and H<sub>2</sub> produced the RSR proceeds to the right**



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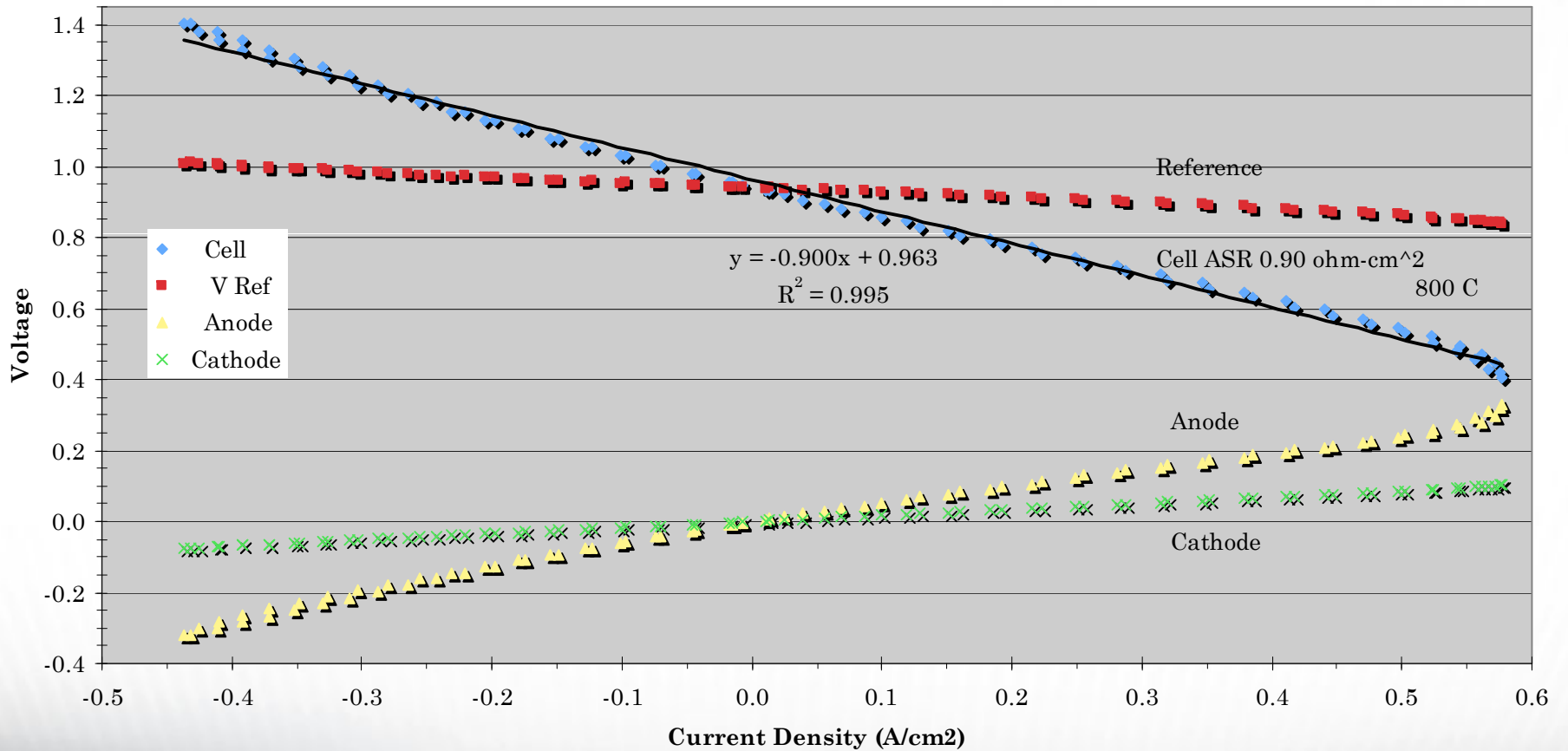
# Wet/Dry CO<sub>2</sub> Electrolysis Cell V-I Comparison

## Cell COCO2-01 Baseline Hydrogen Performance



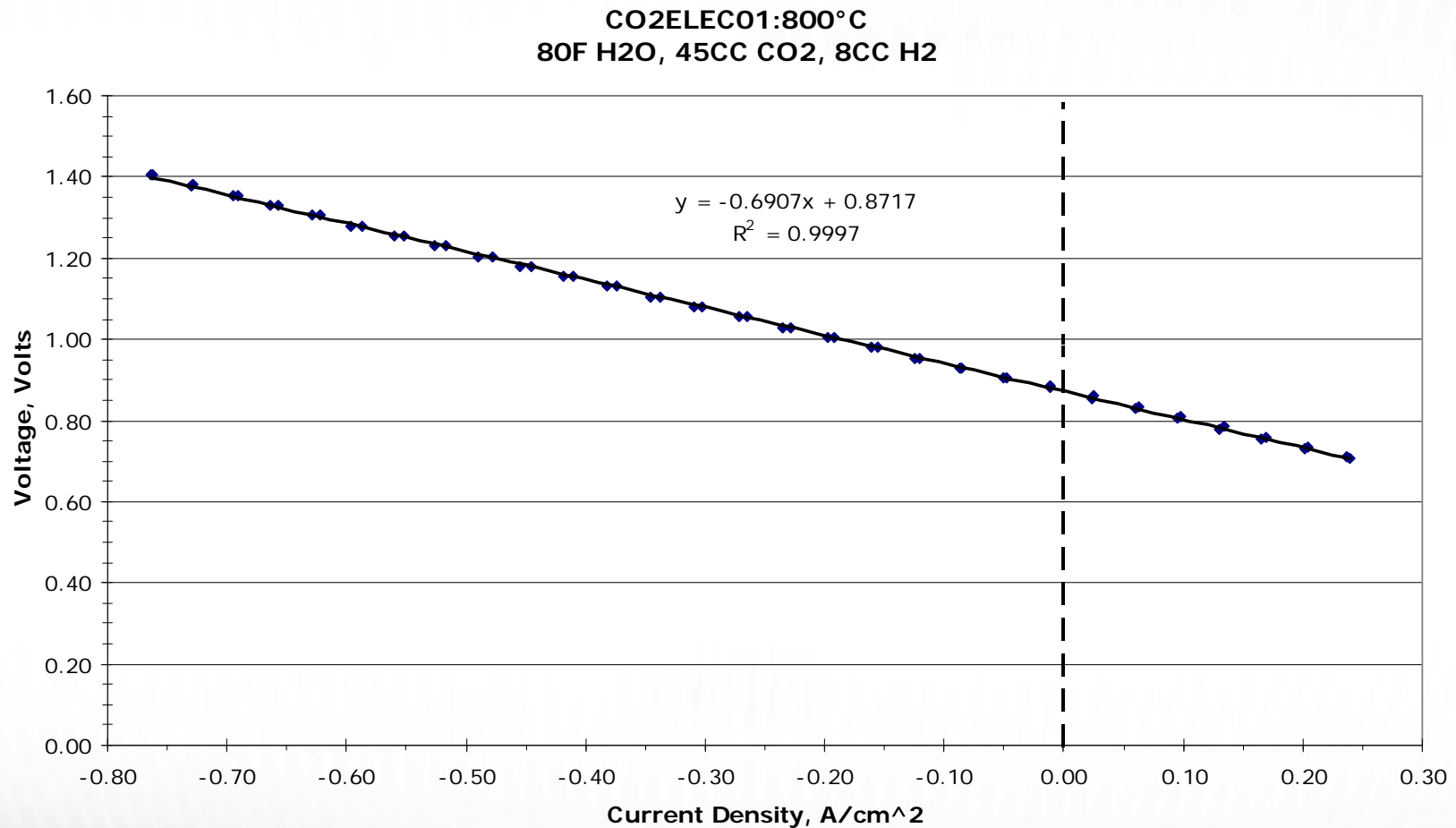
# Wet/Dry CO<sub>2</sub> Electrolysis Cell V-I Comparison

## Dry CO<sub>2</sub> Electrolysis/FC Sweep



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# Humidified CO<sub>2</sub> Cell V-I Characteristic



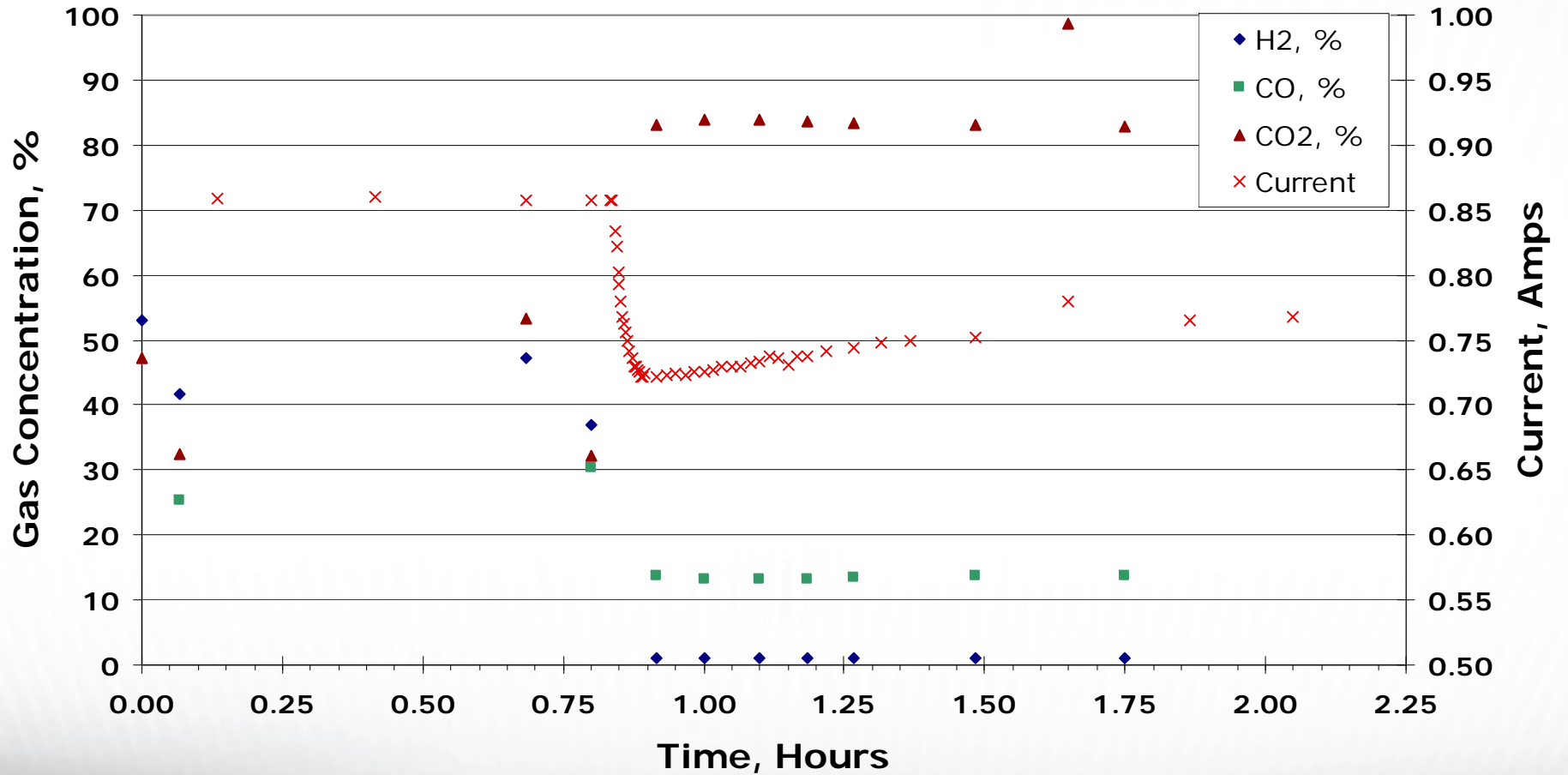
No reduction in performance compared to cells with steam electrolysis



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# Wet to Dry Transient

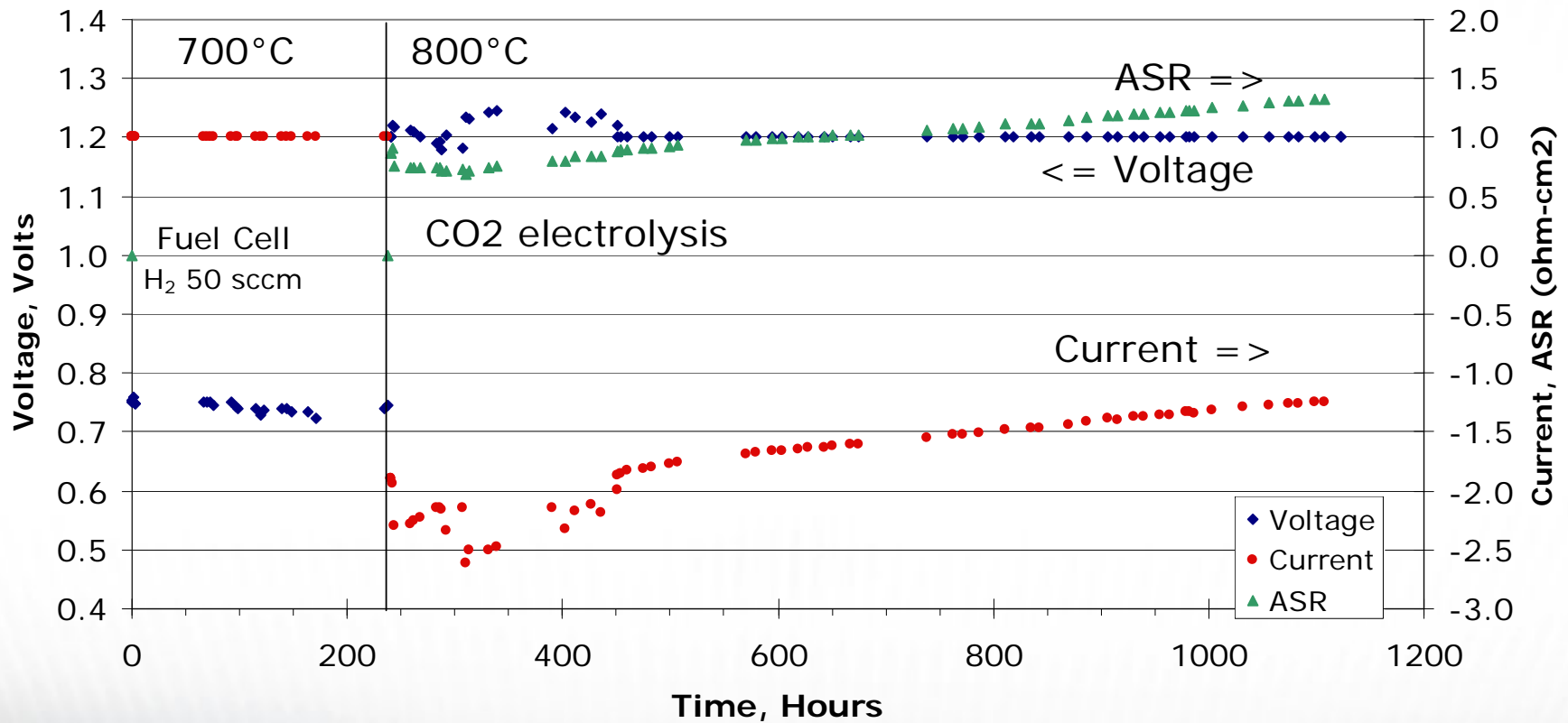
COCO2-05: GC Sweep  
load voltage at -1.2Volts



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# 1100 Hour CO<sub>2</sub> Electrolysis Operation

Cell Gallate146  
CO/CO<sub>2</sub>, 3% H<sub>2</sub>O

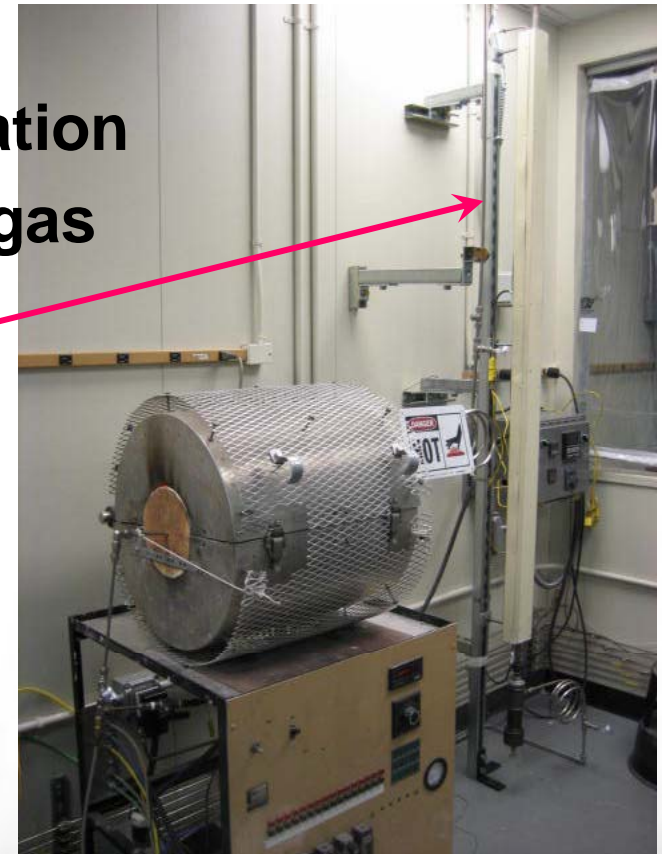


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# Ceramatec laboratory scale FT unit

- Syngas production and storage
  - co-electrolysis of steam and carbon dioxide
- Reforming/Methanation catalyst
- Synthesis gas compressors installation
- FT liquids test run on compressed gas

Fixed bed FT column



- **Caution: Maintain Ni catalyst  
T > ~300° C to avoid highly  
toxic Ni(CO)<sub>4</sub> formation**



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# Syngas Compression and Storage Facility



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# Synthetic methane from electrolysis of CO<sub>2</sub>

Gas analysis in volume %

	From Electrolysis			From FT Unit		
	CH <sub>4</sub>	CO	H <sub>2</sub>	CH <sub>4</sub>	CO	H <sub>2</sub>
Test 1	.0	14.3	60.7	42.5	0	13.8
Test 2	.7	18.5	58.0	47.7	0	9.2
Test 3	.3	20.1	63.5	50.0	0	9.4
Test 4	.1	15.8	58.9	42.0	0	4.6
Test 5	.1	15.2	59.5	40.4	0	8.2

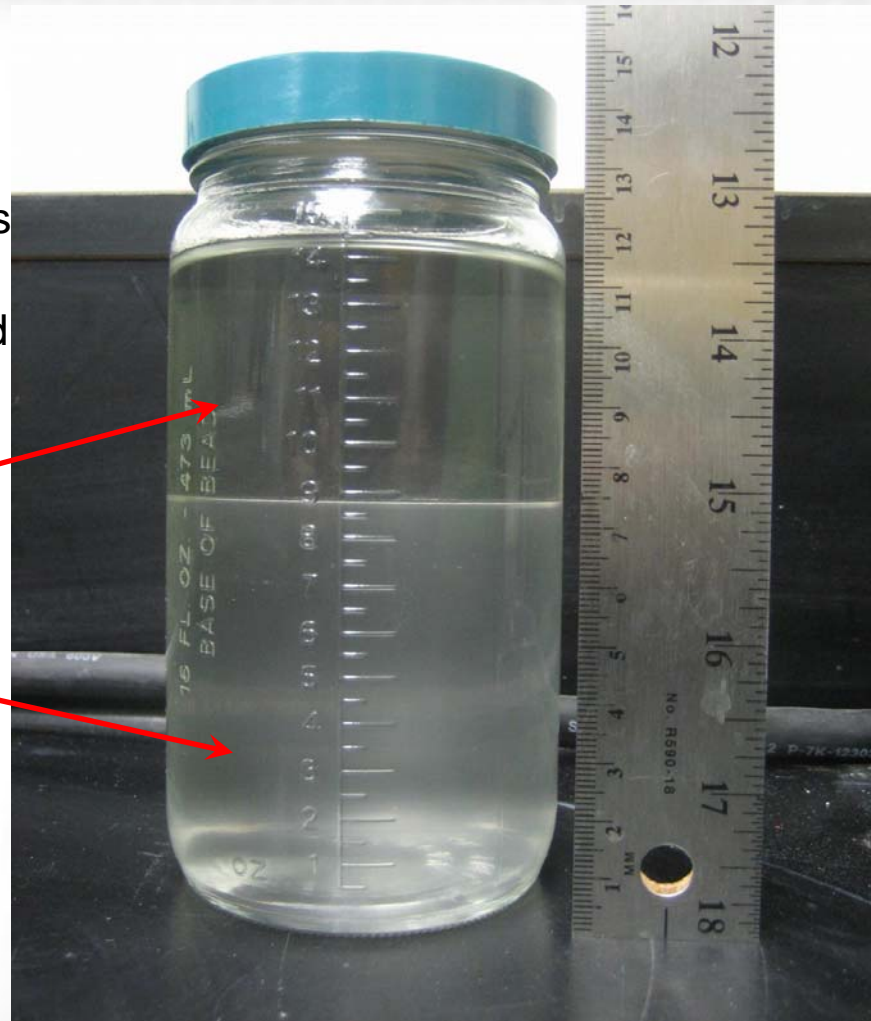
***FEED TO ELECTROLYSIS IS CO<sub>2</sub> + H<sub>2</sub>O + ELECTRIC ENERGY***



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# FT- Liquid Products

- Ceramatec produced catalyst
  - FeCuK composition
  - 8mm La promoted alumina rings
  - Automated in-situ reduction profile using dewpoint controlled temperature ramp
  
- Oil fraction
- Water fraction



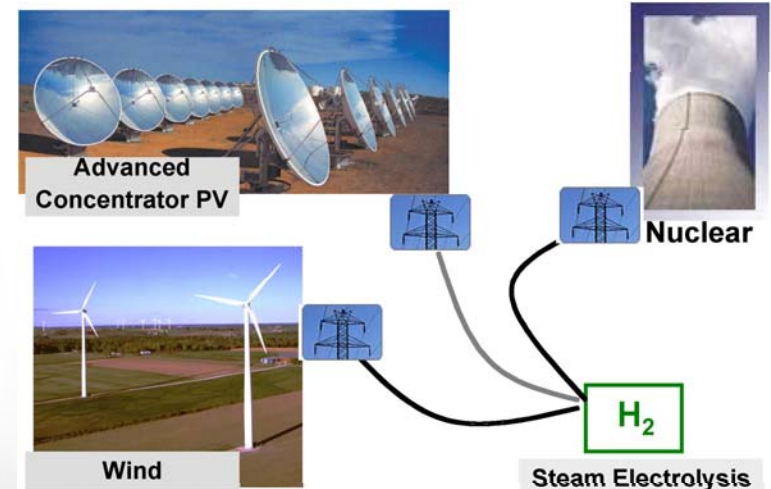
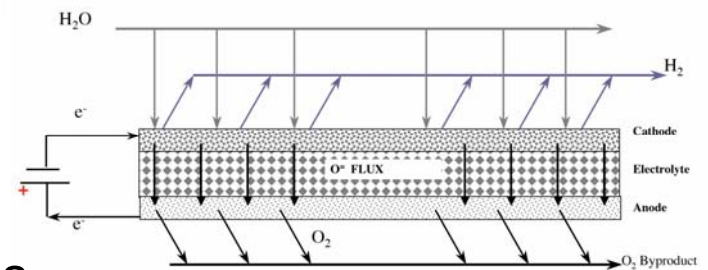
235° C Reactor Operation



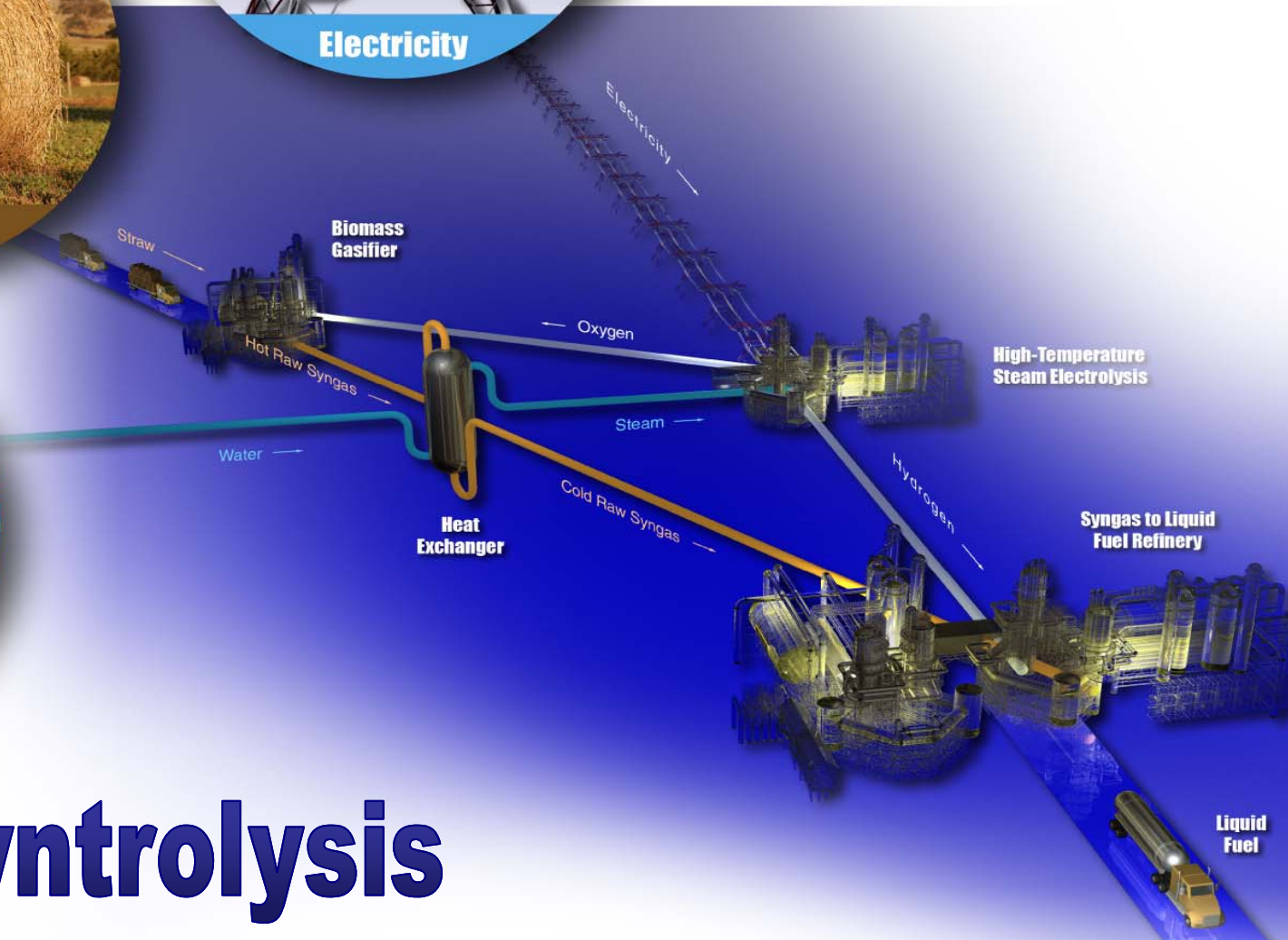
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# High Temperature Electrolysis

- Leverage decades of SOFC R&D
- Inputs
  - $e^-$  (green electrons)
  - steam  $\Rightarrow$  hydrogen
  - co-electrolysis of  $H_2O + CO_2 \Rightarrow$  syngas
  - heat input optional, depends on operating point
- Most efficiency means of hydrogen production
  - $e^-$  to hydrogen
    - $\eta=100\%$  at 1.285V
    - $\eta=95\%$  at 1.35V
    - $\eta=107\%$  at 1.20V, (heat required)
- Hot  $O_2$  and steam byproduct
  - Valuable for biomass gasification

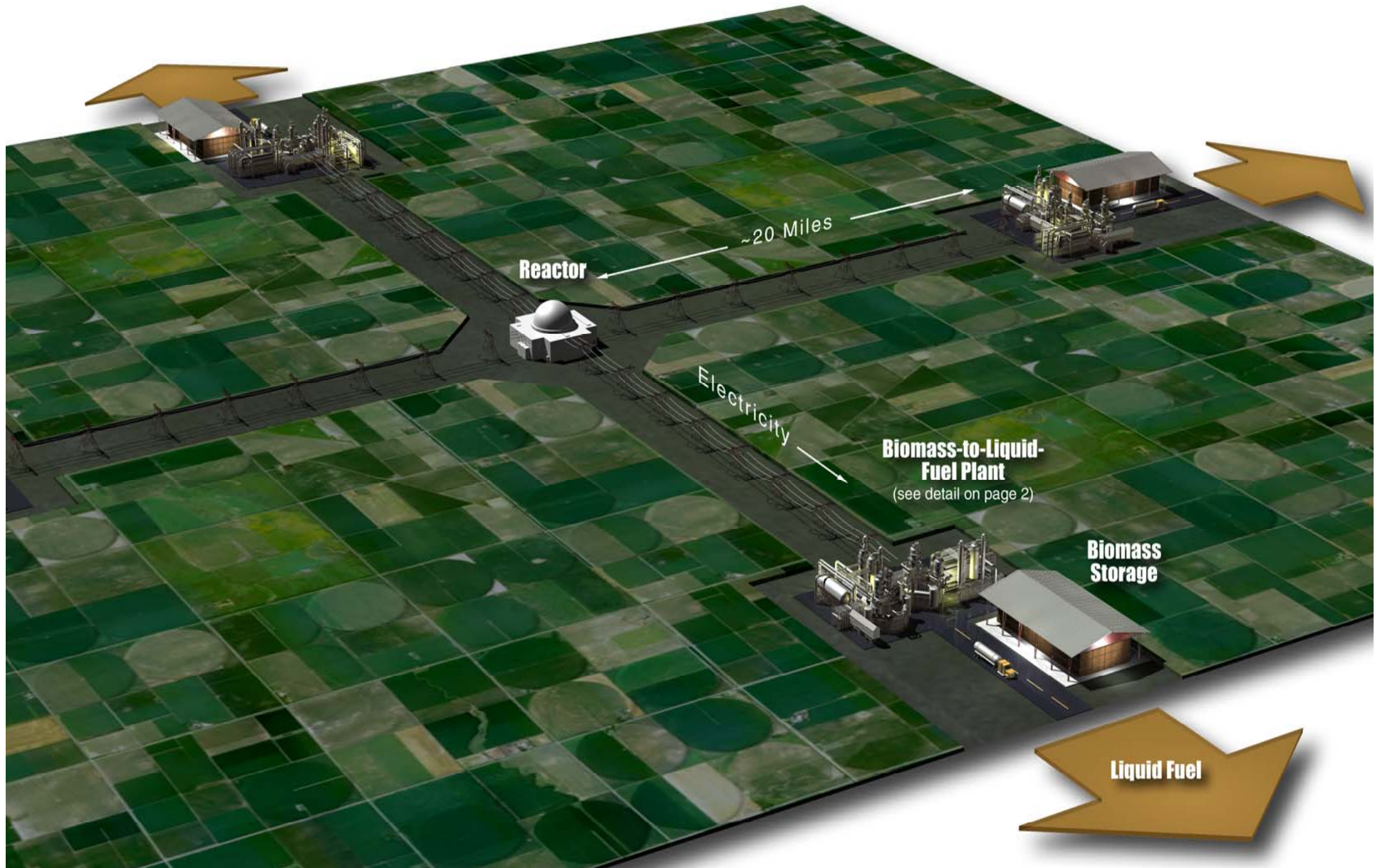


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# Bio-Syntrolysis

# Bio-Syntrolysis: Regional Concept



# What Can Be Produced on 40x40 Miles?

- Biomass Feedstock
  - 22,700 annualized TPD dry biomass (8.1 Tons/acre)
    - 10,000 TPD C, 1,400 TPD H from cellulose
- Wind Energy
  - 5 MW/km<sup>2</sup> wind turbine density over 1600 square miles
  - 20 GW wind power potential (only need 5 to 7 GW for fuel)
- Electrolytic Hydrogen or Syngas
  - 3,300 TPD H<sub>2</sub> required for all biomass C to fuel
  - 1800 gpm net water consumption after rev-shift & FT
- Synfuel
  - 30,000 bbl/day biomass to liquids + 24 kTPD CO<sub>2</sub>
  - Additional 58,000 bbl/day combining CO<sub>2</sub> and electrolysis
    - 4.7 GW with HTE or 6.5GW with water electrolysis



# Synergies

- **Grid Stabilization**
  - Non-dispatch nature of wind/solar
    - Limits wind to small % of total generation mix
    - More nuclear for H<sub>2</sub> enables more wind for H<sub>2</sub>
  - Dispatch controlled electrolysis loads
    - More power => more hydrogen => lower cell efficiency
    - Less power => less hydrogen => higher cell efficiency
    - Increase fraction of wind in total generation mix
- **Transmission Backloading**
  - Wind often at end of line, rural site
  - Co-locate load and production
  - Co-locate electrolysis and biomass gasifier



# Conclusions

- Hydrogen may be finely tuned via HTE to obtain desired CO/H<sub>2</sub> syngas ratio for fuel processing
- Source of pure, high temperature, oxygen greatly reducing nitrogen containing pollutants
- All process heat for HTE is supplied by gasifier
- If electricity is powered by non-fossil sources, the process is carbon neutral
- HTE technology may be scaled to small distributed biomass processing units to reduce transportation cost of biomass gathering
- Syngas production efficiencies between 70% to 80% may be achieved



# Conclusions

- Over 90% of the carbon in the biomass is converted to syngas resulting in low carbon dioxide emissions during fuel processing
- Higher carbon-to-hydrogen ratios in the biomass provide for better carbon conversion
- Low mass heating value promotes a high syngas production efficiency



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